



# cdmHUB.org

## The Composites Design & Manufacturing HUB:

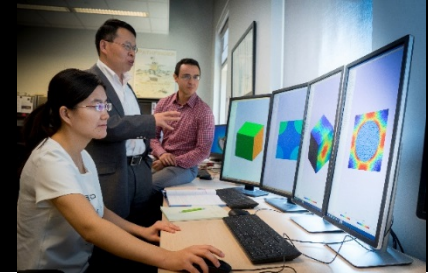
A Platform for Pervasive  
Composites Learning in the  
Cloud

R. Byron Pipes  
Wenbin Yu  
Johnathan Goodsell

**PURDUE**  
UNIVERSITY

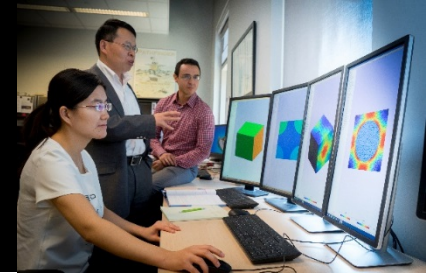
**COMPOSITES  
DESIGN &  
MANUFACTURING  
HUB**

# The Vision

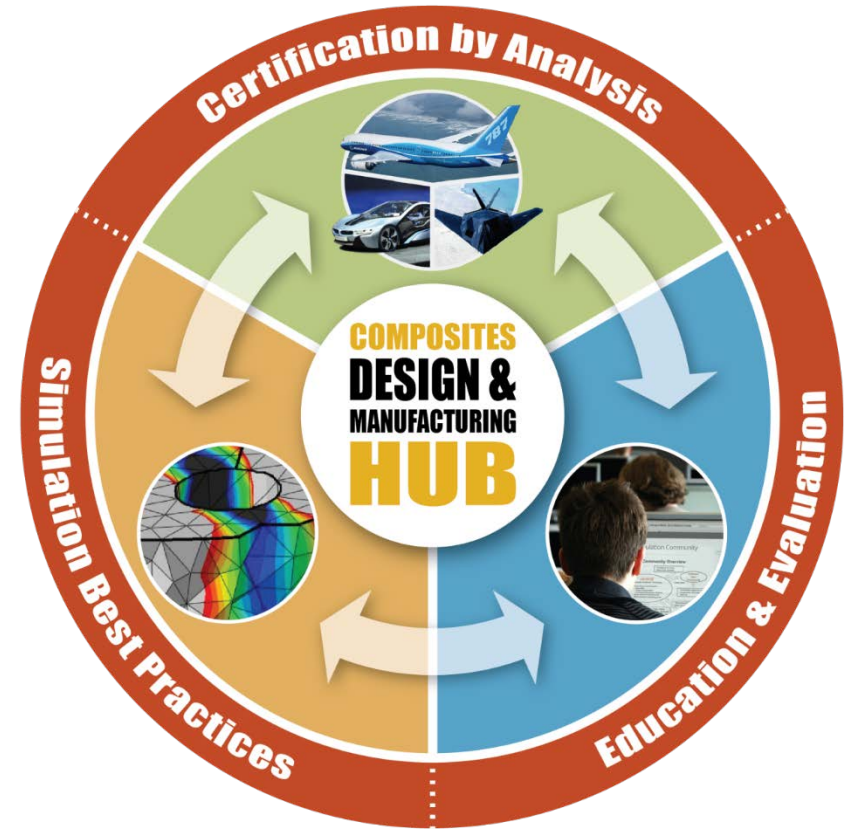


- Simulation can *provide the foundation* for a revolution in composites design, manufacturing and certification
- *Finger tip access* to composites simulation tools anywhere anytime on any devices - real commercial codes connected to HPC resources in the cloud.
- *Certifying* composite product manufacturing and performance *by simulation* is clearly within reach
- *Accelerated pervasive learning* about composites and the tools necessary for their design

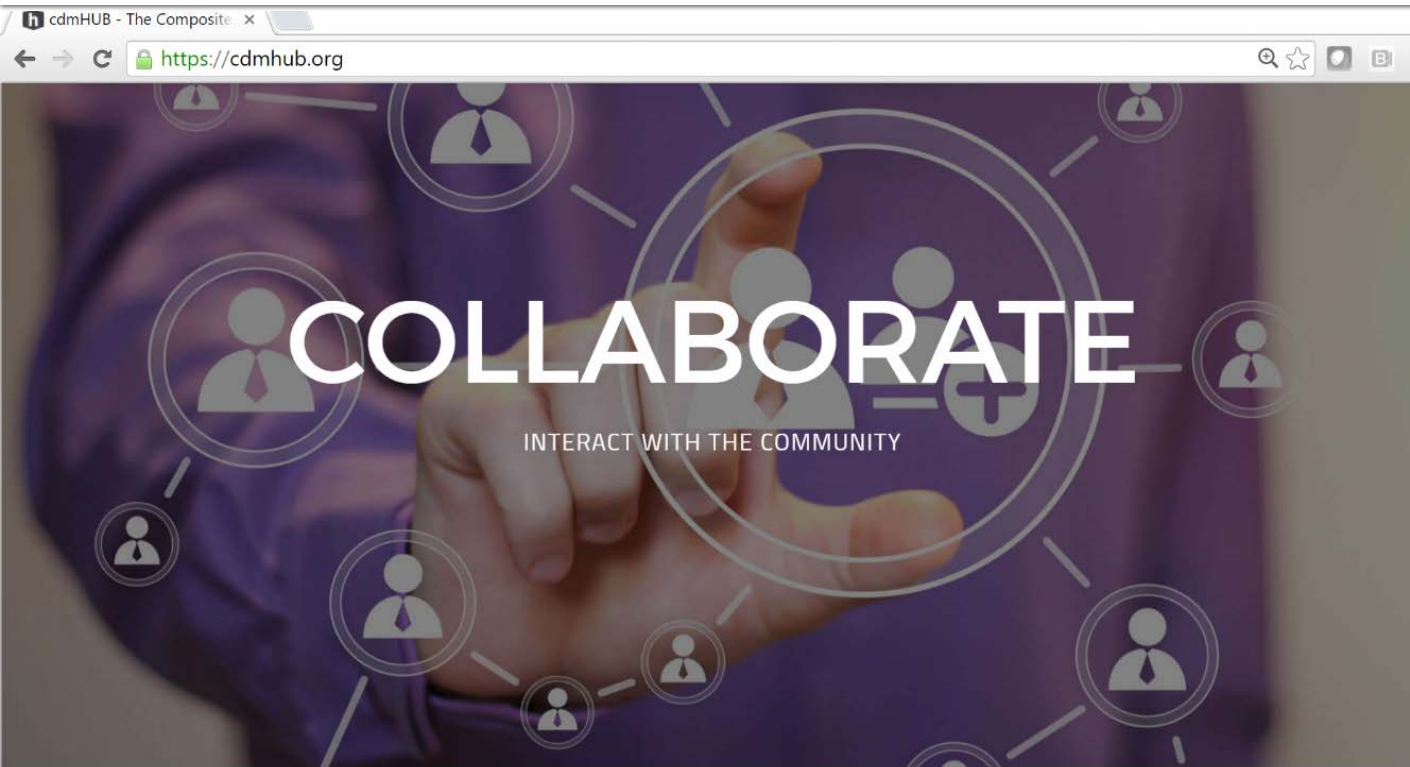
# The Mission



Convene the composites community to advance **certification by analysis** by education and evaluation of composites simulation tools and establishing simulation best practices.



# The Online Composites Community



*Over  
2000  
Users to  
Date!*

*On our  
way to  
10,000!*

WE ARE

the composites community of designers,  
manufacturers, researchers, engineers,

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# cdmHUB Platform Overview

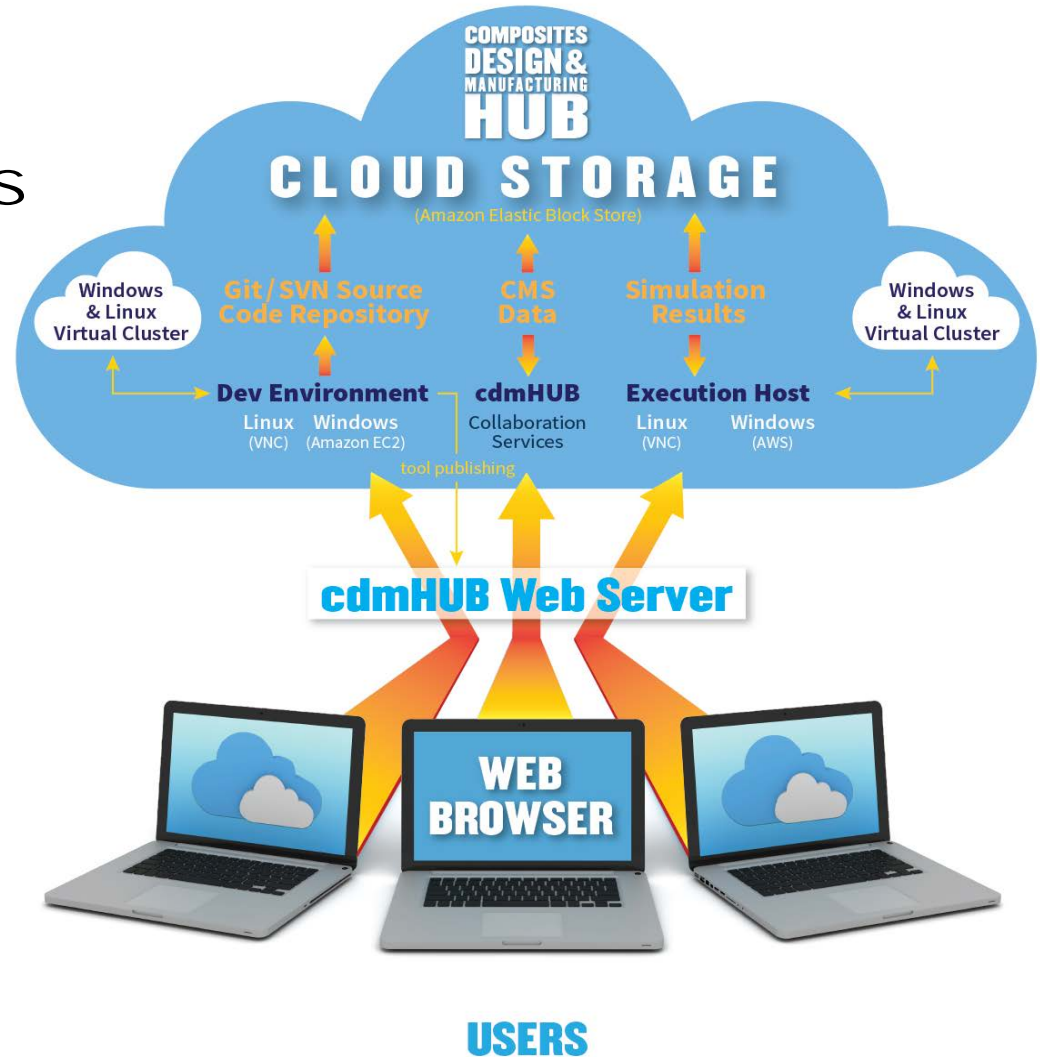
Collaboration Services

Dev Environment

Execution Host

HPC

Cloud storage



Researchers | Engineers | Manufacturers | Educators



# cdmHUB Goals

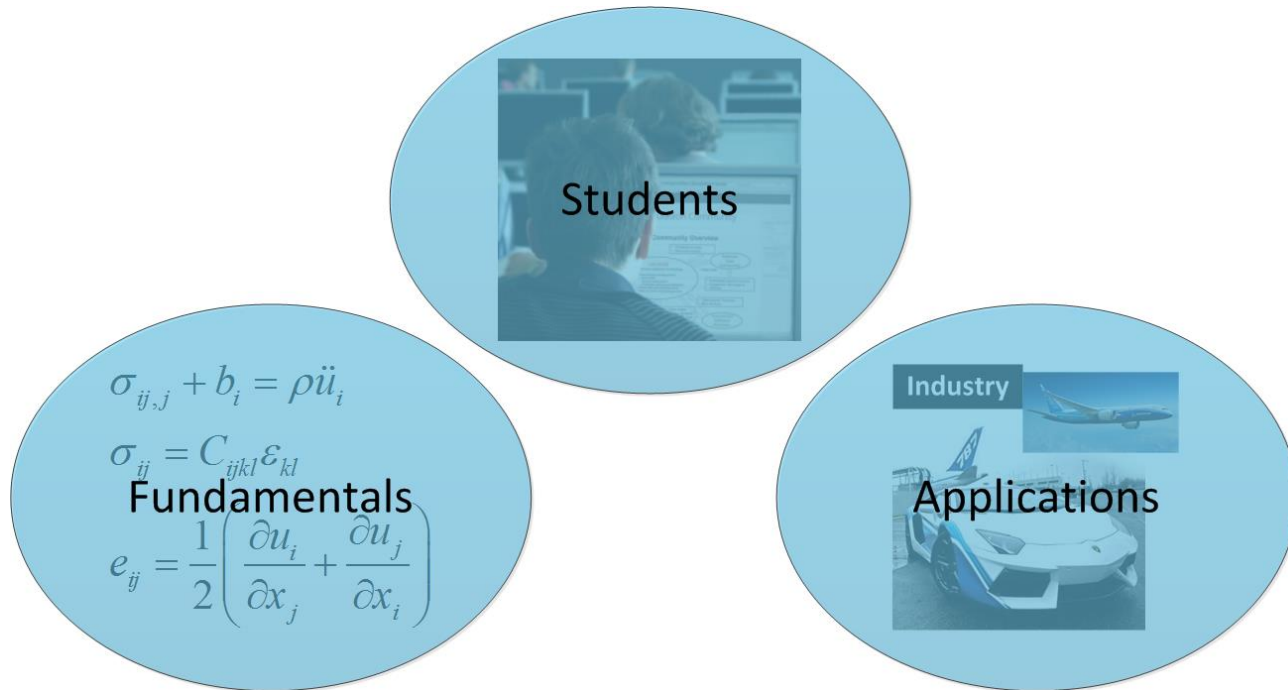


- Increase in the rate of development and deployment of composites simulation tools and the user community **by an order of magnitude**
- Launch a platform
  - Host and integrate existing simulation tools
  - Create a new array of simulation tools
  - Develop the human talent to support composites design and manufacturing simulation
- Create for composites
  - Virtual classroom
  - Virtual lab
  - Virtual factory

# Benefits to the cdmHUB Community

- Education in the use of composites simulation tools:
  - *What tools are available?*
  - *What tool is best for a specific problem?*
  - *What are the tool functionalities?*
  - *How is a particular tool connected with other tools?*
- Tool development for manufacturing and processing simulation
- Expert evaluation of simulation tool taxonomy and Tool Maturity Level (TML)
- Establishment of protocols for simulation tool validation and verification (V&V)
- Access to data sets required for TML and V&V

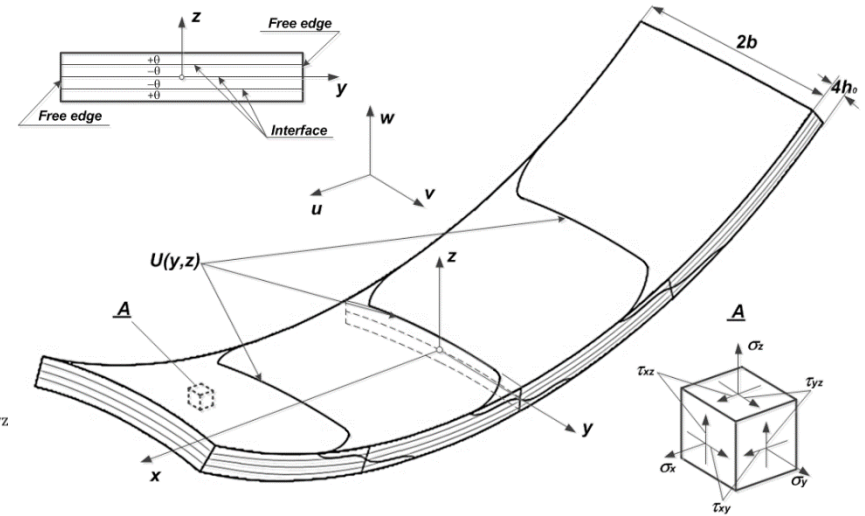
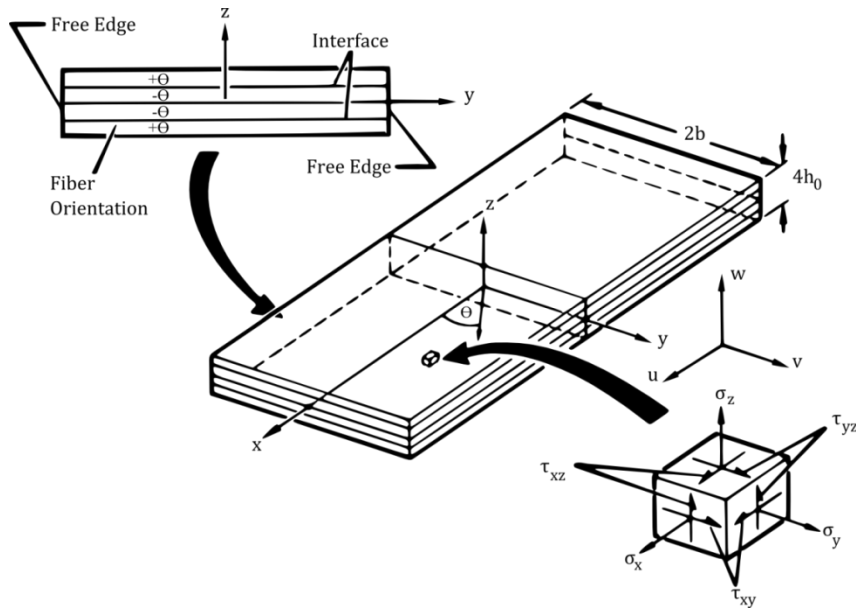
# Simulation Tools Advance Composites Education



Simulation Tools enable Students to connect the Fundamentals to the Applications



# The Pipes-Pagano "Free-Edge" Interlaminar Stress Problem



Pipes, R. B. and Pagano, N. J., "Interlaminar Stresses in Composite Laminates Under Uniform Axial Extension," J. Comp. Matl., 1970

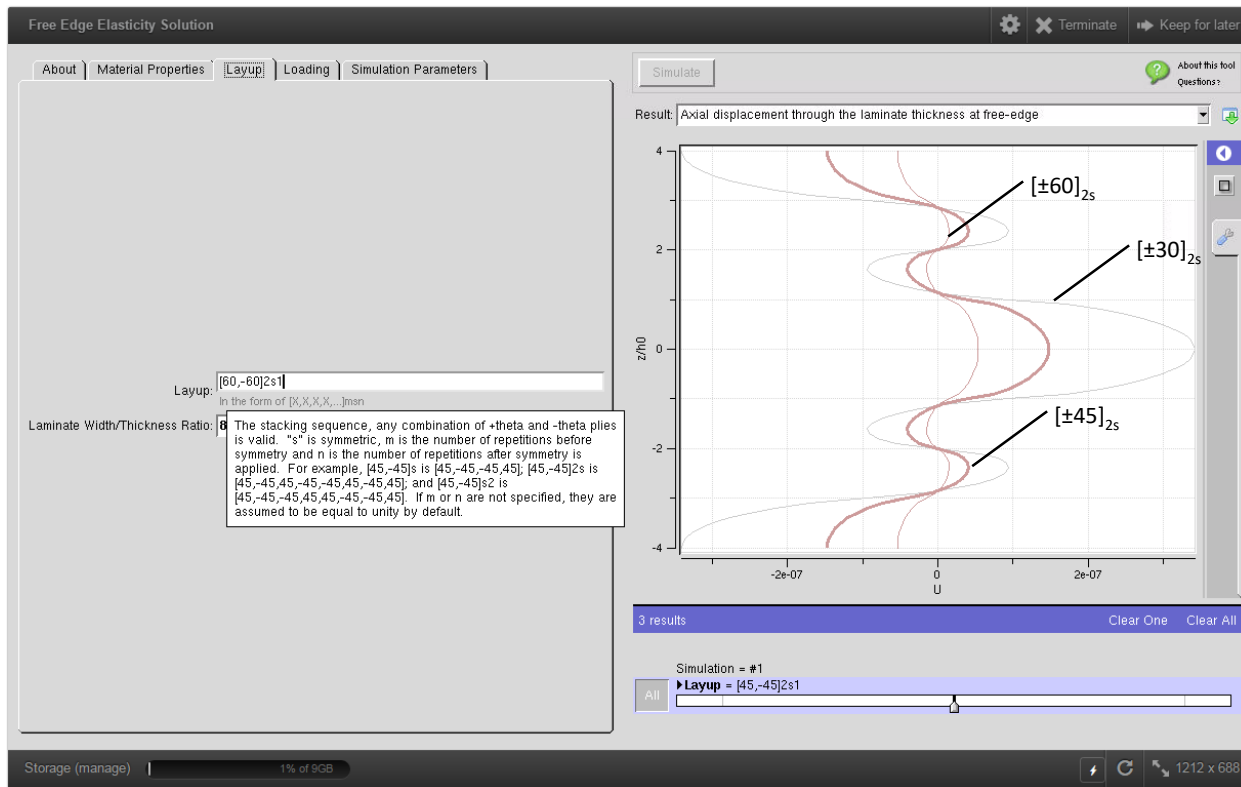
Pipes, R. B., and Pagano, N. J., "Interlaminar Stresses in Composite Laminates-An Approximate Elasticity Solution," J. App. Mech., 1974

Goodsell, J., Pipes, R.B., "Interlaminar Stresses in Angle-Ply Laminates: a Family of Solutions," Journal of Applied Mechanics, Vol. 83, No. 5, (2016).

Pipes, R. B., Goodsell, J., Ritchey, A., Dustin, J., and Gosse, J., "Interlaminar Stresses in Composite Laminates: Thermoelastic Deformation," Comp. Sci. Tech., 2010

Goodsell, J., Pagano, N. J., Kravchenko, O., and Pipes, R. B., "Interlaminar Stresses in Composite Laminates Subjected to Anticlastic Bending Deformation," J. App. Mech., 2013

# Multiple solutions at your fingertips



# Accelerate Exploration and Learning

$$U(y, z) = \sum_{n=1}^{\infty} \frac{2\alpha^{1/2}}{n\pi\nu^2} \Lambda_k \frac{e^{-\nu\alpha^{-1/2}(b-y)} - e^{-\nu\alpha^{-1/2}(b+y)}}{1 + 2e^{-2\nu\alpha^{-1/2}b}} \cos \nu \left( z + \frac{mh_0}{2} \right)$$

$$U_y(y, z) = \sum_{n=1}^{\infty} \frac{2}{n\pi\nu} \Lambda_k \frac{e^{-\nu\alpha^{-1/2}(b-y)} + e^{-\nu\alpha^{-1/2}(b+y)}}{1 + 2e^{-2\nu\alpha^{-1/2}b}} \cos \nu \left( z + \frac{mh_0}{2} \right)$$

$$U_z(y, z) = -\sum_{n=1}^{\infty} \frac{2\alpha^{1/2}}{n\pi\nu} \Lambda_k \frac{e^{-\nu\alpha^{-1/2}(b-y)} - e^{-\nu\alpha^{-1/2}(b+y)}}{1 + 2e^{-2\nu\alpha^{-1/2}b}} \sin \nu \left( z + \frac{mh_0}{2} \right)$$

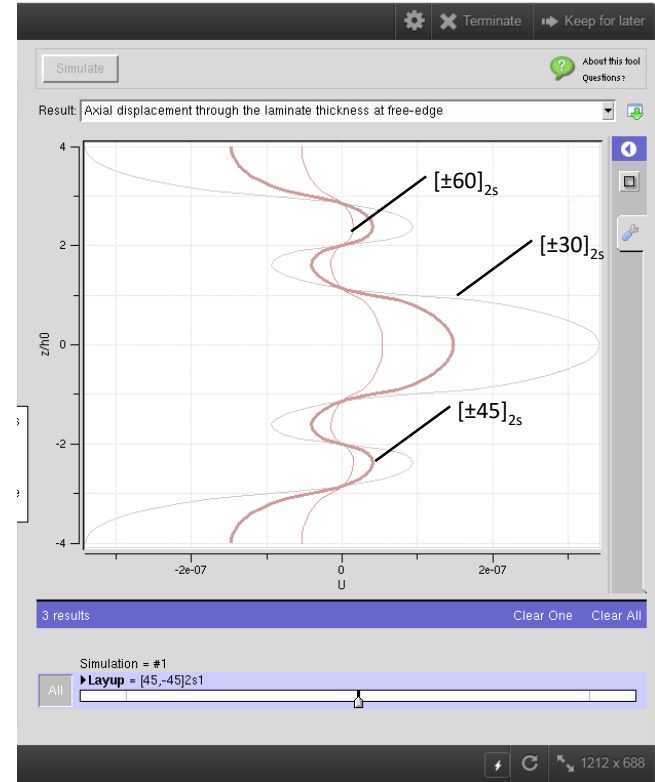
$$\nu = \frac{n\pi}{mh_0}$$

$$\Lambda_k = \sum_{k=1}^m \left\{ \begin{array}{l} \nu(\Phi_E + \Phi_T) \left[ \sin \nu \left( z + \frac{mh_0}{2} \right) \right]_{(k-1)h_0}^{kh_0} \\ + \Phi_B \left[ \cos \nu \left( z + \frac{mh_0}{2} \right) + \nu z \sin \nu \left( z + \frac{mh_0}{2} \right) \right]_{(k-1)h_0}^{kh_0} \end{array} \right\}$$

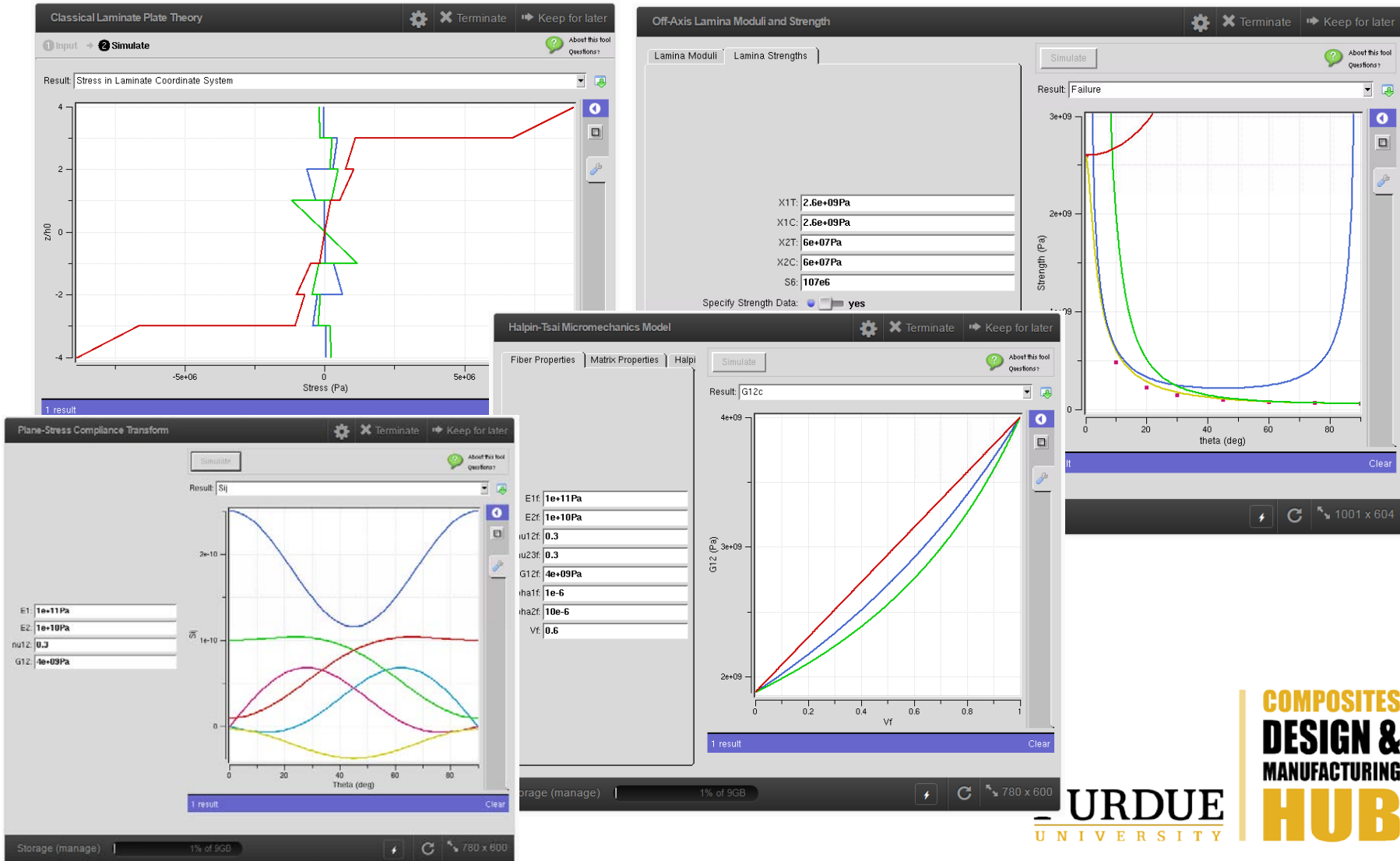
$$\Phi_E = \frac{S_{16}}{S_{11}} \varepsilon_0$$

$$\Phi_T = \frac{S_{55}}{\alpha S_{66}} \alpha_{xy} \Delta T$$

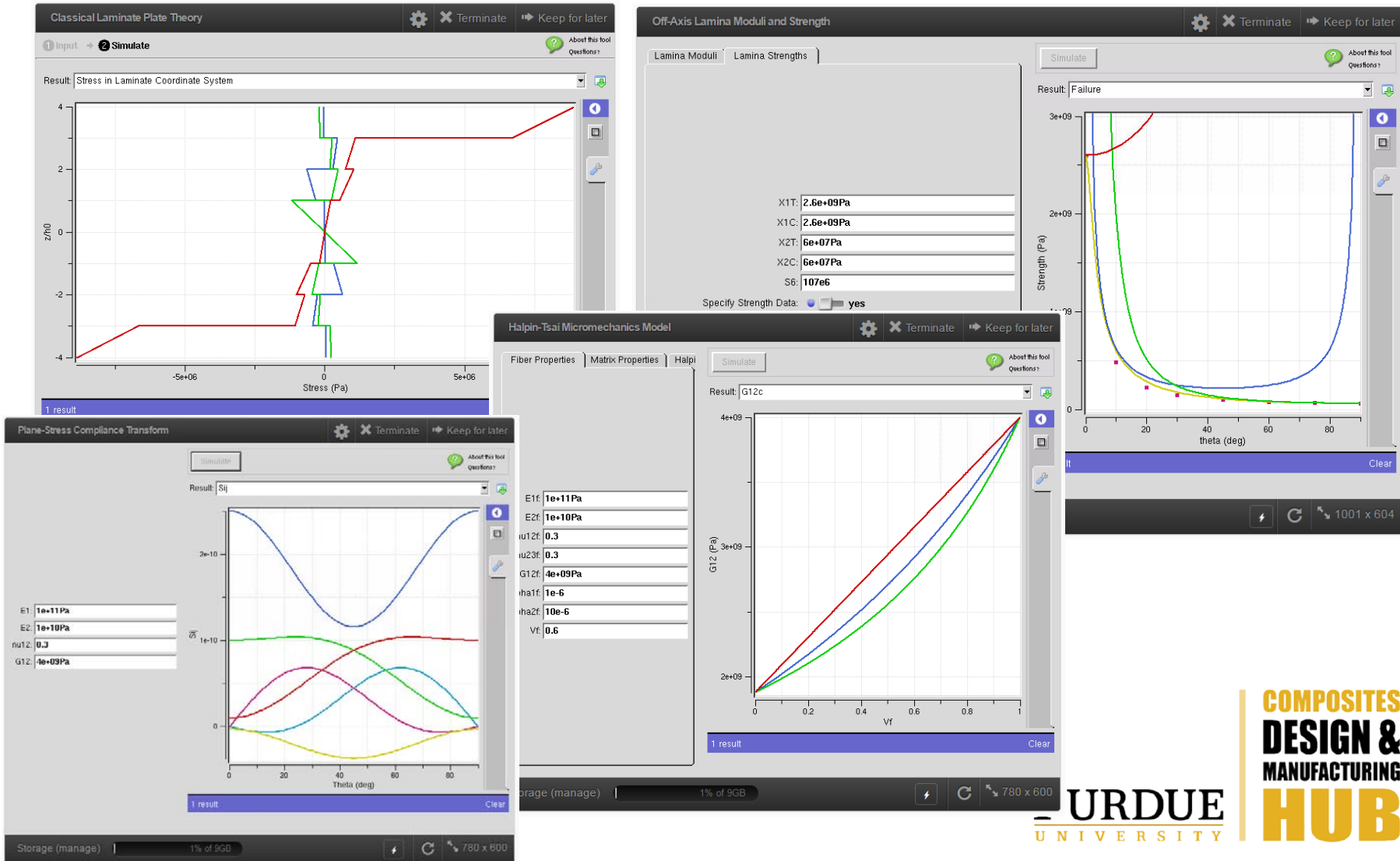
$$\Phi_B = \frac{S_{16}}{S_{11}} \kappa_x$$



# Composites Fundamentals

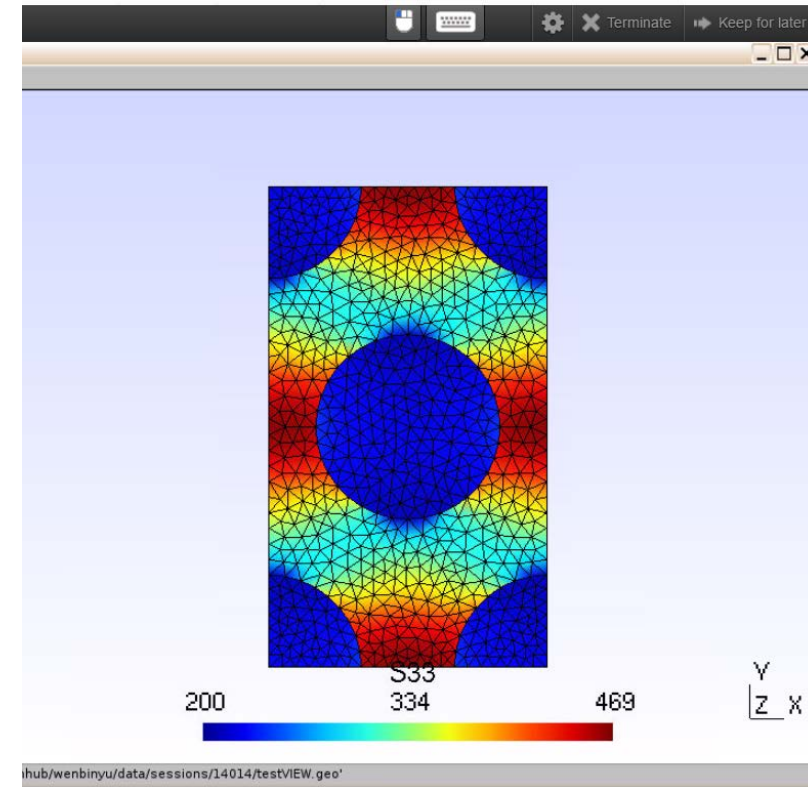


# Composites Fundamentals



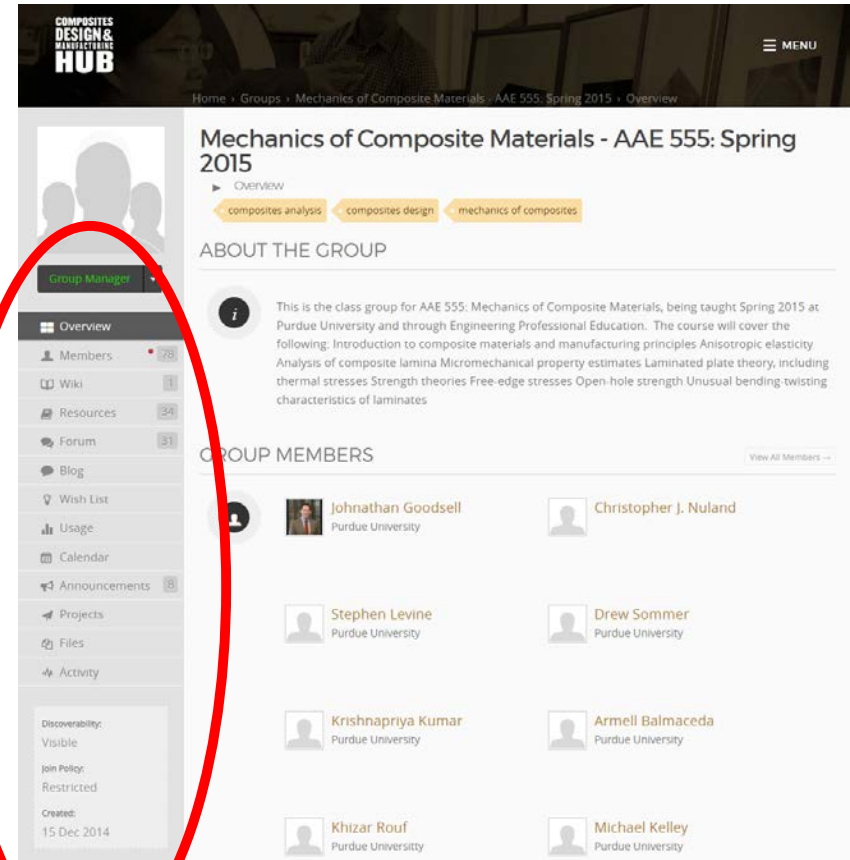
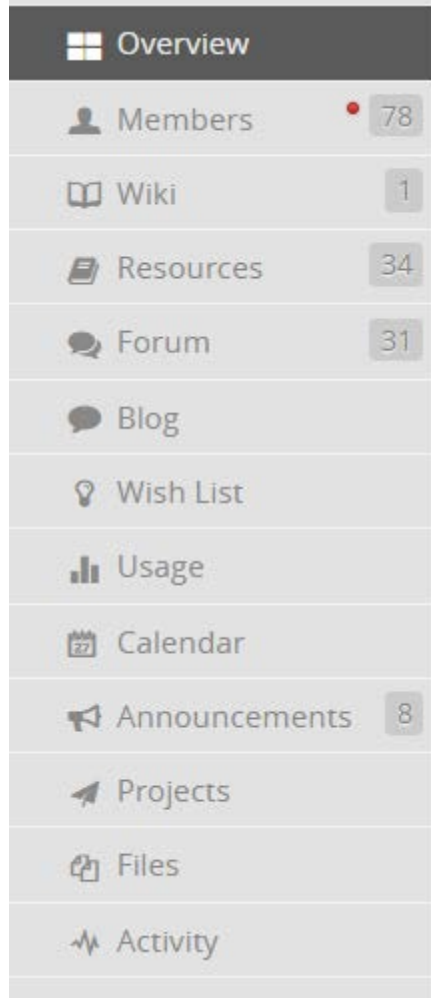
# And More...

Classical Composites Analysis	Advanced Composites Analysis	Processing
Classical Laminate Plate Theory	Free Edge Elasticity Solution	Autocatalytic Degree of Cure (Cure Kinetics)
Effective Lamina and Laminate Properties	Geometrically Exact Beam Theory	DiBenedetto Equation ( $T_g$ )
Fiber Spacing and Volume Fraction	LAMMPS (Molecular Dynamics)	
Fiber Volume Fraction	SwiftComp	
G_to_K Orthotropic Conversion & K_to_G Conversion	SwiftComp Pro	
Halpin-Tsai Micromechanics Model	Variational Asymptotic Beam Analysis	
Laminate Failure Analysis	Viscoelastic Shear Lag	
Off-Axis Lamina Moduli and Strength		
Plane-Stress Compliance Transform		



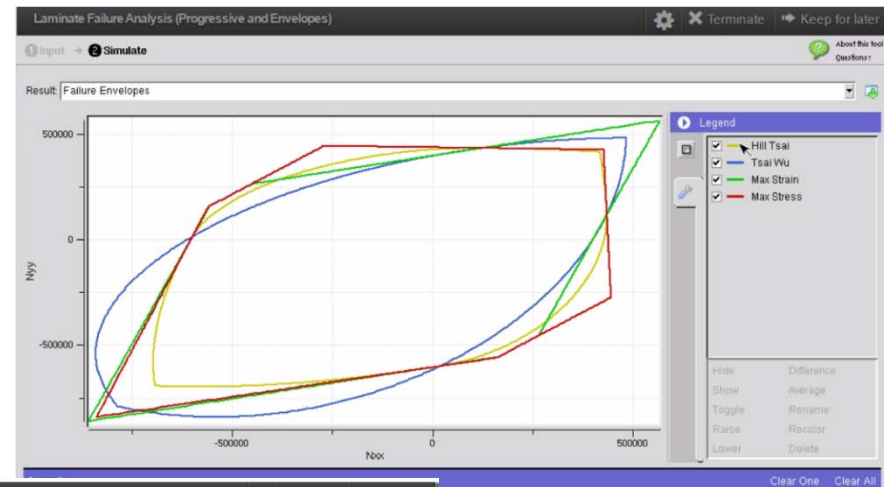


# A Full-Range of Course Management Features



# Mechanics of Composite Materials

- Anisotropic Elasticity
- Lamina Analysis
- Micromechanics
- Classical Laminated Plate Theory
- Elementary Damage and Failure
- Interlaminar Stresses



**Free Edge Elasticity Solution**

About | Material Properties | Layout | Loading | Simulation Parameters

Simulate new input parameters

**Angle-Ply Free-Edge**

This tool calculates an approximate elasticity solution for a finite width angle-ply laminate subjected to uniform axial extension, uniform temperature change and anticlastic bending. The x-axis is aligned with the axial extension direction, the y-axis is the transverse in-plane direction and the z-axis is the through thickness coordinate. The solution is uniform along the x-axis because the laminate is assumed to have infinite dimension in this direction. The stress, strain and displacement are solved for using a Fourier series representation in the y-z plane. The boundary layer width may be calculated. The solution is valid for general angle-ply (+theta, -theta) laminates; no restrictions on the symmetry of the stacking sequence or on equal numbers of +theta and -theta plies need be imposed.

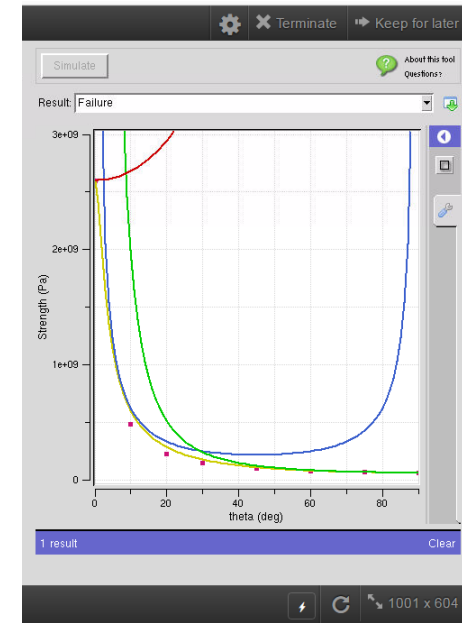
For reference see:

- Pipes, R.B. and Pagano, N.J., "Interlaminar Stresses in Composite Laminates - An Approximate Elasticity Solution," Journal of Applied Mechanics, Vol. 41, No. 3, (1974), pp. 668-672.
- Pipes, R.B., Goodsell, J., Ritchey, A., Dushin, J., Gosse, J., "Interlaminar Stresses in Composite Laminates: Thermoelastic Deformation," Composites Science and Technology, Vol. 70 (2010), pp. 1805-1811.
- Goodsell, J., Pagano, N.J., Kravchenko, O., Pipes, R.B., "Interlaminar Stresses in Composite Laminates Subjected to Anticlastic Bending Deformation," Journal of Applied Mechanics, in press.

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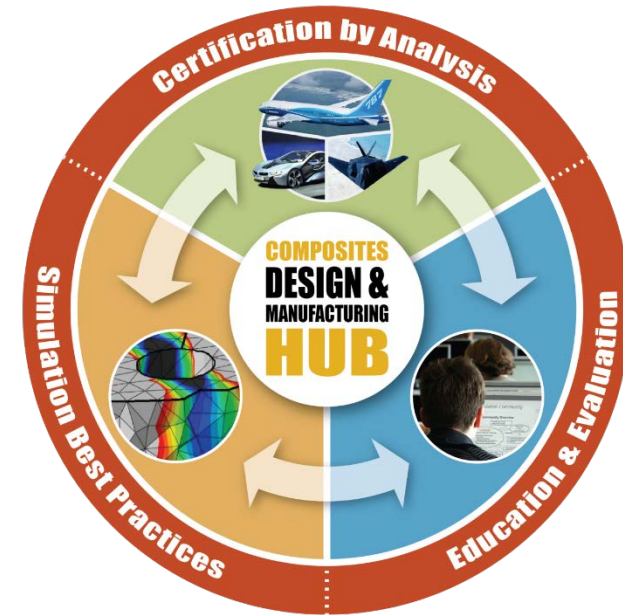
# Experimental Characterization of Advanced Composite Materials

Experiment	Output
Microscopy	Fiber volume fraction, fiber spacing, void content
0-degree and 90-degree tension	Lamina tensile moduli: $E_1, E_2, \nu_{12}$ Lamina tensile strengths: $X^T, Y^T$
$\pm 45$ -degree tension	Lamina shear moduli: $G_{12}$ Lamina shear strength: $S$
Off-axis tension (often 10-degree, 30-degree, 45-degree and 60-degree)	Lamina off-axis modulus, $E_x$ Lamina biaxial strength
Laminate tension (often $[0/\pm 45/90]_s$ , $[0/\pm 45/0]_s$ , $[\pm 25]_s$ , etc...)	Laminate tensile modulus: $E_x$ Laminate uniaxial tensile strength
Lamina thermoelastic	Lamina coefficients of thermal expansion: $\alpha_1, \alpha_2$
Laminate thermoelastic	Laminate coefficients of thermal expansion: $\alpha_x, \alpha_y, \alpha_{xy}$
Lamina and laminate flexure	Lamina and laminate flexure modulus Lamina and laminate flexure strength
Laminate open-hole tension	Laminate open-hole strength
Lamina double-cantilever beam (DCB)	Mode I energy release rate, $G_{Ic}$
Lamina end-notch flexure (ENF)	Mode II energy release rate, $G_{IIc}$



# Closing Remarks

1. Simulation can accelerate learning, in both a theory and experimental-based course
2. Education must address the “what-to” and the “where-to/when-to” as well as the “how-to”
3. Simulation must be grounded in validation
4. The cdmHUB provides tools and a platform for the above



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